

Shop Tips

NOVEMBER, 1963

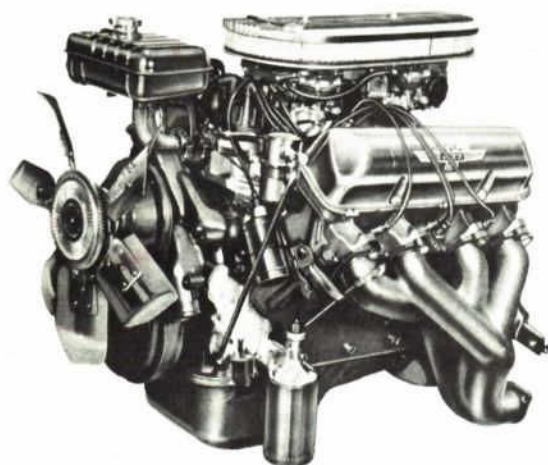
FROM FORD

VOL. 1, NO. 2

Technical parts and service information published by Ford Division to assist servicemen in Service Stations, Independent Garages and Fleets.



SPECIAL FEATURE!



1963-64 FORD 427 C.I.D. HIGH PERFORMANCE ENGINE SPECIFICATIONS • PARTS ACCESSORIES

(See page 3)

Be sure to file this and future bulletins for ready reference. If you have any suggestions for additional information that you would like to see included in this publication, please write to: Ford Division of Ford Motor Company, Parts and Service Promotion and Training Dept., P. O. Box 658, Dearborn, Michigan, 48121.

IN THIS ISSUE

Article	Title	Page
1	Engine Oil Warning System—Vehicles Equipped with 427 C.I.D. Engines	2
2	Complete List of 1964 Power Options	2
3	Ford 427 High Performance Engine Specifications	3
4	Ford 427 High Performance Engine Service Parts	4
5	Miscellaneous High Performance Accessories	6
6	Lightweight Body Components	6
7	Generator Failure from Road Splash—1963 F-100-250-350 Trucks	7
8	Vinyl Trim Cleaning Materials	7
9	Steering Linkage Service Requirements on 1963 Thunderbird and Falcon	7
10	Disc Wheel Nut Loosening Ford 500 Through 800 Series Trucks	7
11	Revisions in Rear Axle Bolt Torque Specifications—1963 Vehicles	8
12	Exhaust System Clearance—1963 Falcon with V-8 Engine	8
13	Distributor Modification for Improved Low End Acceleration and Fuel Economy and Carburetor Modification for Improved Fuel Economy—1963 Ford with 352 Engine and 2V Carburetor	8
14	Increased Engine Idle Speed—1963 144-170 Passenger Car Engines with Automatic Transmissions	10
15	Hydraulic Tappet Noise—Diagnosis and Testing	10
16	New Cylinder Head Gasket, Head Bolt Washers and Head Bolt Specifications—1958 Through 1963-401, 477, 534 Engines	10
17	Surging or Hesitation—1963 Econoline with 144 or 170 Engine	10
18	Clutch Snap Ring Failure—Fordomatic Two-Speed Transmissions	11
19	Clutch Snap Ring Failure—1961 Through 1963 Cruise-O-Matic Transmissions	11
20	Carburetor Percolation or Excessive Pressure Build-Up in Fuel Line—1954-62 Cars	12

(Continued on Page 2)

From your Ford dealer



IN THIS ISSUE—Continued

Article	Title	Page
21	Spark Plug Flashover During Compression Test on Spark Plug Testers	12
22	Spark Plug Replacement—1962 and 1963 Fairlane with 221 and 260 C.I.D. Engines	12
23	Distributor Testing of Transistor Ignition—427 High Performance and Super Duty Truck Engines—1963	13
24	Service Replacement Radio Speakers—Ford Cars and Trucks	13
25	Instrument Panel Gauge Readings—1963 Vehicles with AM-FM Radio	13
26	Radio Control Breakage—Tone, Volume, On-Off Switches—1963 Vehicles	13
27	Loose Tachometer Head—1963 Falcon Sprint	14
28	Tachometer Installation on Standard Ignition Engines	14
29	Tachometer Application to Transistorized Ignition System	14
30	Turn Signal Switch Not Cancelling—1963 Ford with Automatic Transmission	15
31	Seat Belts (Metal to Metal Type)—Proper Threading—1963 All Car Lines	15
32	Fuel Line Vibration (Fuel Pump to Carburetor) 1963-221, 260 and 289 C.I.D. Engines	15
33	Improved Automatic Choke Operation and Fuel Economy on Short Trip Stop and Go Type Driving—221, 260, 352, 390 C.I.D. Engines	16

1 ENGINE OIL WARNING SYSTEM—Vehicles Equipped With 427 C.I.D. Engines

A new engine oil warning system was released and is being used on all Ford 427 C.I.D. engines. This system now warns the driver of either a loss of oil pressure or excessive oil temperature. The system has an oil pressure sending unit and an oil temperature sending unit (both located on top of the oil filter adapter). It also has an oil temperature relay and oil temperature flasher assembly (both located above the master brake cylinder under the hood assembly), and a new wiring harness. The warning light has not been changed and is still located in the instrument panel cluster.

The operation of this system is as follows:

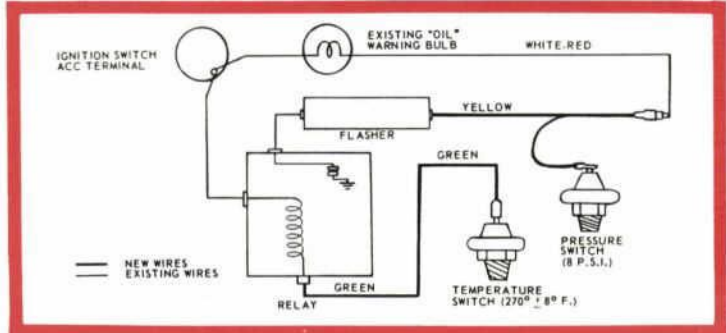
When the oil temperature rises above $270^{\circ} \pm 8^{\circ}$ F., the instrument panel oil indicator light will flash on and off until the oil temperature drops below the $270^{\circ} \pm 8^{\circ}$ F. temperature.

When the oil pressure drops below the required 8 PSI the same instrument panel oil indicator light will now glow continuously.

The following wiring diagram and warning light operation chart will aid in servicing this new system:

OIL WARNING LIGHT OPERATION CHART

Oil Temperature	Oil Pressure	Light Operation
Below $270^{\circ} \pm 8^{\circ}$ F.	Below 8 P.S.I.	ON
Below $270^{\circ} \pm 8^{\circ}$ F.	Above 8 P.S.I.	OFF
Above $270^{\circ} \pm 8^{\circ}$ F.	Above 8 P.S.I.	Flashing On & Off



2 COMPLETE LIST OF 1964 POWER OPTIONS

CAR LINE	ENGINES					TRANSMISSIONS				
	Cu. In.	HP	Cyl.	Carb.	Type of Fuel	3-Speed Manual Column Shift	4-Speed Manual Floor Shift	3-Speed Manual Overdrive	Fordomatic 2-Speed	Cruise O-Matic 3-Speed
FALCON	144	85	6	1-V	REGULAR	STD	—	—	—	—
	170	101	6	1-V	REGULAR	STD	OPT	—	OPT	—
	200	116	6	1-V	REGULAR	—	—	—	*OPT	—
FALCON HI-PERFORMANCE	260	164	V-8	2-V	REGULAR	STD	OPT	—	OPT	—
FAIRLANE	170	101	6	1-V	REGULAR	STD	—	—	—	—
	200	116	6	1-V	REGULAR	—	—	—	*OPT	—
	260	164	V-8	2-V	REGULAR	STD	—	OPT	OPT	—
	289	195	V-8	2-V	REGULAR	STD	OPT	—	—	OPT
FAIRLANE HI-PERFORMANCE	289	271	V-8	4-V	PREMIUM	—	*OPT	—	—	—
FORD	223	138	6	1-V	REGULAR	STD	—	OPT	—	OPT
	289	195	V-8	2-V	REGULAR	STD	—	OPT	—	OPT
	352	220	V-8	4-V	REGULAR	STD	—	—	—	OPT
	390	300	V-8	4-V	PREMIUM	STD	OPT	OPT	—	OPT
	Interceptor 390	330	V-8	4-V	PREMIUM	STD	OPT	—	—	OPT
FORD HI-PERFORMANCE	427	410	V-8	1-4-V	SUPER PREMIUM	—	*OPT	—	—	—
	427	425	V-8	2-4-V	SUPER PREMIUM	—	*OPT	—	—	—
THUNDERBIRD	390	300	V-8	4-V	PREMIUM	—	—	—	—	STD

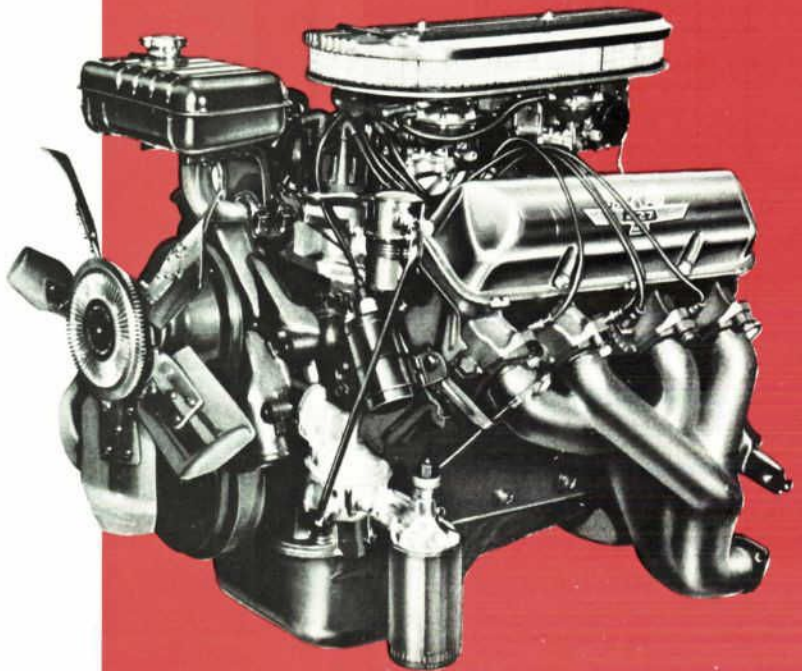
*Required at Additional Cost



1963-64 FORD *HIGH PERFORMANCE* PARTS AND ACCESSORIES

On the following pages is a list of engine and chassis parts that are available from Ford dealers to service Ford vehicles with the 427 cubic inch High Performance engine.

This handy reference guide is designed to make it easy for you to identify parts which may be required for servicing vehicles with the 427 engine or prepare them for various competitive activities.



3

1963-64 FORD 427 ENGINE SPECIFICATIONS

Bore.....	4.23 in.
Stroke.....	3.78 in.
Firing order:.....	1-5-4-2-6-3-7-8
Maximum B.H.P.....	410 @ 5600 RPM 8-V
	425 @ 6000 RPM 4-V
Maximum Torque.....	476 @ 3400 RPM 8-V
	480 @ 3700 RPM Nominal 10.9:1 Maximum 11.5:1
Compression Ratio:.....	
Camshaft, Part No. C2AE-6250-A (Std.)	
Intake opens.....	8° 30' ATC*
Intake closes.....	36° 30' ABC*
Exhaust opens.....	11° 30' BBC*
Exhaust closes.....	39° 30' BTC*
Valve overlap.....	96°
Contact point settings.....	.018-.022 (dwell angle 33 to 35)

Spark Plug Recommendations.....	COAZ-12405-A COAZ-12405-B
Spark Plug Gap.....	Street Use: .032 Racing: .025
Ignition Timing.....	8°
Valve lash.....	.025-.028 Hot
Fuel Pump Pressure.....	5 to 6 lbs. at 1800 RPM (No Load)
RPM Red Line.....	6200 RPM
Carburetor Jets.....	8-V—Primary 62 Fixed Power .040
Valve Spring Pressure.....	80 to 90 lbs. at (replace below 70)
Valve Spring compressed to 1.320.....	1.820 length 255 to 280 lbs.

*Figures based on 8-V engine



1963-4 Ford High Perf

4

Part Number	Description	Part Number	Description	Part Number	Description
FRONT SUSPENSION AND STEERING LINKAGE		ENGINE (Continued)		ENGINE (Continued)	
C1AA-1177-A	Oil Seal, Rear Wheel Bearing Inner	C3AZ-6135-A	Pin—Piston	C3AZ-6531-A	Support—Rocker Arm (4V and 8V)
C0AZ-3102-A	Spindle, Right Hand	C3AZ-6140-B	Retainer, Piston Pin	C3AZ-6A536-A	Seat Valve Spring 4V—8V
C0AZ-3103-A	Spindle, Left Hand	C3AZ-6148-A	Partial Ring Set—Std. Size 4V—8V	B6A-6549-C	Screw, Valve Rocker Arm Adjusting 4V—8V
C0AA-3280-C	Rod Assembly—Spindle Arm	C3AZ-6200-C	Rod Assy.—Connecting 4V—8V	C3AZ-6563-A	Shaft, Valve Rocker Arm 4V—8V
C1AA-3289-D	End, Spindle Arm	C3AZ-6200-F	Rod Assy.—Connecting Reinforced Cap 4V—8V	B8A-6564-B	Arm Assy. Valve Rocker 4V—8V
C0AA-3304-D	Rod Assembly—Idler Arm	C1AE-6211-H-J	Bearing, Connecting 4V—8V	B8A-6565-C	Rod—Valve Push 4V—8V
AG-3310-A	Sleeve Assembly Drag Link	C2AZ-6214-A	Bolt—Connecting Rod 4V—8V	B8A-6571-B	Seal—Valve Stem 4V—8V
C0AA-3351-A	Bracket Idler Arm Mtg	C3AZ-6250-D	Camshaft (306°) 4V—8V	EAA-6572-A	Plug—Valve Rocker Arm Shaft 4V—8V
C0AA-3355-A	Arm Idler	C3AZ-6250-K	Camshaft (324°) 4V—8V	C3AZ-6582-F	Cover Assy. Valve Rocker Arm R.H. 4V—8V
LF-3357-A	Bushing, Idler	C3AZ-6256-A	Sprocket—Camshaft (4V and 8V)	C3AF-6582-G	Cover Assy. Valve Rocker Arm L.H. 4V—8V
30AA-3590-D	Arm, Pitman	B8A-6262-AA	Bearing Camshaft Intermediate (4V and 8V)	B9AE-6584-C	Gasket, Valve Rocker Arm 4V—8V
REAR AXLE		B8A-6263-AA	Bearing Camshaft Rear (4V and 8V)	B8A-6587-B	Spring, Valve Rocker Arm Locating 4V—8V
C1AW-4209-E	Kit—Diff. Gear and Pinion (5.83)	C3AZ-6265-A	Spacer Cam Sprocket (4V and 8V)	B8A-6590-A	Washer, Valve Rocker Arm Shaft 4V—8V
WAB-4209-C	Kit—Diff. Gear and Pinion (5.67)	B8S-6267-AA	Bearing Camshaft Front Intermediate (4V and 8V)	B8A-6598-A	Washer, Valve Rocker Arm Shaft Spring 4V—8V
WAB-4209-D	Kit—Diff. Gear and Pinion (5.43)	C3AZ-6261-A	Bearing Camshaft Front (4V and 8V)	C3AZ-6600-A	Pump Assy. Oil 4V—8V
WAB-4209-E	Kit—Diff. Gear and Pinion (5.14)	B8A-6268-A	Chain—Timing (Link-Belt) (4V and 8V)	B8A-6608-A	Rotor & Shaft Assy. Oil Pump Drive 4V—8V
WAB-4209-F	Kit—Diff. Gear and Pinion (4.86)	B8A-6270-AA	Bearing—Camshaft Rear Intermediate (4V and 8V)	B8A-6616-C	Cover, Oil Pump 4V—8V
WAB-4209-G	Kit—Diff. Gear and Pinion (4.71)	C3AZ-6269-A	Plate Camshaft Thrust (4V and 8V)	B8AZ-6A618-A	Shaft Assy. Oil Pump Intermediate 4V—8V
WAB-4209-H	Kit—Diff. Gear and Pinion (4.57)	C3AZ-6287-A	Eccentric, Cam Fuel Pump Drive (4V and 8V)	C0AE-6622-E	Screen & Cover Assy. Oil Pump 4V—8V
WAB-4209-J	Kit—Diff. Gear and Pinion (4.29)	C3AZ-6303-G	Crankshaft—Roller Fillets (4V and 8V)	C2AE-6622-E-SO	Screen & Cover Assy. Oil Pump 8 QT. 4V—8V
WAB-4209-K	Kit—Diff. Gear and Pinion (3.40)	B8A-6306-A	Sprocket, Crankshaft (4V and 8V)	B8A-6626-A	Gasket, Oil Pump Inlet Flange 4V—8V
C0AW-4234-D	Shaft—Rear Axle Right Hand	B8A-6310-A	Slinger-Crankshaft Oil (4V and 8V)	B8A-6629-A	Ring, Oil Pump Shaft Retainer 4V—8V
C0AZ-4235-C	Shaft—Rear Axle Left Hand	C3AZ-6312-B	Damper Assy.—Crankshaft Vibration	B9AZ-6A630-C	Baffle Assy. Crankcase Ventilation 4V—8V
C2AZ-4880-A	Kit—Locking Differential	C1AE-6333-A & B	Bearing Crankshaft Main Front (4V and 8V)	C3AZ-6A630-A	Duct, Crankcase Ventilation 4V
FRONT SPRING AND STABILIZER		C1AE-6336-B	Seal Crankshaft Rear Main Cap (4V and 8V)	C3AZ-6A630-B	Duct—Crankcase Ventilation 8V
AJ-5310-N	Front Spring 750 Lbs	C1AE-6337-A & B	Bearing, Crankshaft Main Center (4V and 8V)	C0AE-6A631-A	Element, Crankcase Ventilation 4V—8V
AJ-5310-R	Front Spring 900 Lbs	C1AE-6345-B	Bolt (4V and 8V)	C1AE-6A632-A	Gasket, Crankshaft Ventilation 4V—8V
C3AZ-5310-F	Front Spring, 1,200 Lbs	C3AZ-6A354-A	Spacer Main Bearing Cap (4V and 8V)	C0AE-6A633-A	Retainer, Crankcase Ventilation 4V—8V
C1AA-5482-A	Stabilizer Bar	B 3765 69		C0AE-6A636-A	Gasket, Oil Filter Adaptor to Block 4V—8V
C0AA-5493-A	Insulator	B 3748 52		C1AZ-6A642-A	Oil Cooler
ENGINE		C 3731 35		B8A-6659-A	Gasket, Oil Pump to Block 4V—8V
C3AE-6007-HE-359-T	Engine Assembly—427 CI—4V	B8AZ-6359-A	Spacer Crankshaft Damper	C0AZ-6666-A	Plug, Cup (Relief Valve) 4V—8V
C3AE-6007-HE-361-T	Engine Assembly—427 CI—8V	C3AZ-6375-E	Flywheel Assembly (4V and 8V)	COME-6670-A	Spring—Relief Valve 4V—8V
B9AE-6A008-A	Dowel—Cylinder Head to Cylinder Block	B8A-6378-A	Washer Crankshaft Damper	C1AE-6670-A	Spring, Oil Pump Relief Valve 4V—8V
C3AZ-6009-K	Cylinder Assembly 427 CI—4V	B8A-6379-A	Bolt Flywheel (4V and 8V)	B9AE-6674-B	Plunger—Relief Valve 4V—8V
C3AZ-6009-M	Cylinder Assembly 427 CI—8V	C3AZ-6392-A	Housing Assembly—Flywheel (4V and 8V)	C1AE-6674-A	Plunger, Oil Pump Relief Valve 4V—8V
C3AZ-6010-K	Cylinder Block 4V and 8V	EAD-6397-A	Dowel Flywheel Hsg to Cyl. Block (4V and 8V)	C0AE-6675-F	Pan Assy. Oil 4V—8V
C2AZ-6019-A	Kit—Cylinder Front Cover—4V—8V	B9TE-6500-A	Tappet Assy. Valve (4V and 8V)	C1AE-6675-F	Pan Assembly—Oil (1962/63 406 & 427 CI)
C0AE-6020-C	Gasket, Cyl. Front Cover—4V—8V Also in (C2AZ-6019-A Kit)	C3AZ-6505-E	Valve, Exhaust (4V and 8V)	C2AZ-6675-A-SO	Pan Assembly—Oil—8 Quart (4V and 8V)
C2AZ-6023-B	Pointer, Timing 4V—8V	C3AZ-6507-J	Valve Intake Bumper Type (4V and 8V)	AE-6677-A	Cover—Starter Pinion
C3AZ-6049-J	Cylinder Head Assy 4V—8V	C3AZ-6513-A	Spring Assy. Valve Damper (4V and 8V)	C3AZ-6700-A	Bearing—Crankshaft—Front Oil
C3AZ-6051-B	Cylinder Head Gasket 4V—8V	C3AZ-6514-A	Retainer—Valve Spring (4V and 8V)	B4Q-6701-A	Seal—Crankshaft—Rear Oil (4V and 8V)
C1AE-6065-A	Bolt—Cylinder Head (Long) 4V—8V	B8A-6518-A	Key Valve Spring Retainer (4V and 8V)	C0AE-6710-C	Gasket, Oil Pan (4V and 8V)
C1AE-6065-C	Bolt—Cylinder Head (Short) 4V—8V	C1SE-6524-A	Baffle, Valve Spring Oil (4V and 8V)	C1AZ-6731-A	Filter Assembly—Oil (4V and 8V)
C3AZ-6108-M	Piston, Eyebrow Type 4V—8V	C1AE-6A527-A	Bolt 1/2-16 x 3.20 attach 6506 to Cylinder Head 6049 (4V and 8V)		
		C1DE-6A527-A	Bolt 1/2-16 x 2.97 attach 6506 to Cylinder Head 6049 (4V and 8V)		

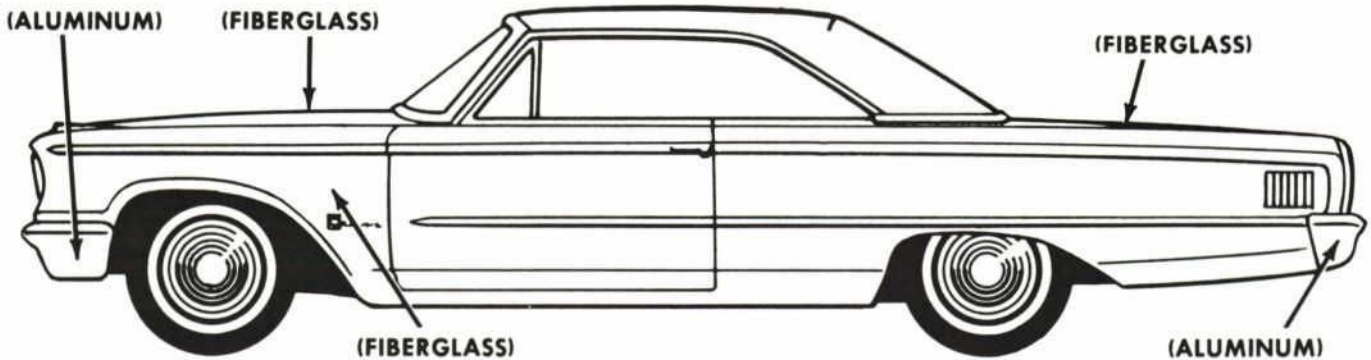


5 MISCELLANEOUS ACCESSORIES



Part Number	Description
C4AZ-5C246-A	Lake Pipe Kit
C4AZ-6B068-A	Engine High Performance Kit
C4AZ-6980-A	Engine Dress-Up Kit
C2RZ-17A326-A	"Sun" Tachometer Kit—8 Cylinder—4"
C2RZ-17A326-B	Rotunda Tachometer—8 Cylinder—4"
C2RZ-17A326-C	Rotunda Tachometer—6 Cylinder—4"
C3RZ-17A326-A	Rotunda Tachometer—6 Cylinder—3"
C3RZ-17A326-B	Rotunda Tachometer—8 Cylinder—3"
C2RZ-17368-A	Bracket Kit for "Sun" Tachometer
C2RZ-17368-B	Bracket Kit for C2RZ-17A326-B and -C Tachometers

6 Lightweight Body Components



PART NUMBER	DESCRIPTION
FOR 1962 GALAXIE SEDAN AND CONVERTIBLE	
C2AB-16005-S	Fender Assy. R.H. (Fiber Glass)
C2AB-16006-S	Fender Assy. L.H. (Fiber Glass)
C2AB-16610-F	Hood Assy. (Fiber Glass)
C2AB-17A867-C	Arm Rear Bumper Outer R.H. (Aluminum)
C2AB-17A868-C	Arm Rear Bumper Outer L.H. (Aluminum)
C2AB-17787-A	Arm Rear Bumper Inner R.H. (Aluminum)
C2AB-17788-A	Arm Rear Bumper Inner L.H. (Aluminum)
C1AB-17A820-A	Brace Frt. Bumper Outer (Aluminum)
C1AB-17A821-A	Brace Frt. Bumper Outer (Aluminum)
C2AB-17757-A	Bar—Frt. Bumper, Impact (Aluminum)
C2AB-17A971-A	Arm, Frt. Bumper Inner R.H. (Aluminum)
C2AB-17A972-A	Arm, Frt. Bumper Inner L.H. (Aluminum)
C2AB-6240110-D	Dr. Assy. Luggage Compt. (Fiber Glass)

PART NUMBER	DESCRIPTION
FOR 1963 GALAXIE SEDAN AND CONVERTIBLE	
C3AA-16005-R	Fender Assy., Front R.H. (Fiber Glass)
C3AA-16006-R	Fender Assy., Front L.H. (Fiber Glass)
C3AA-16044-C	Apron, Front Fender Less W/Strip R.H. (Fiber Glass)
C3AA-16045-C	Apron, Front Fender Less W/Strip L.H. (Fiber Glass)
C3AA-16610-F	Hood Assy. (Fiber Glass)
C3AB-17754-C	Arm, Front Bumper Outer—R.H. (Aluminum)
C3AB-17755-C	Arm, Front Bumper Outer—L.H. (Aluminum)
C3AB-17757-J	Bar, Front Bumper Impact (Aluminum)
C3AB-17795-E	Arm, Rear Bumper Outer R.H. (Aluminum)
C3AB-17796-E	Arm, Rear Bumper Outer L.H. (Aluminum)
C3AB-17906-J	Bar Rear Bumper Impact (Aluminum)
C3AA-6240110-G	Dr. Assy. Luggage Compt. (Fiber Glass)

7 GENERATOR FAILURE FROM ROAD SPLASH—1963 F-100-250-350 Trucks with 30 Amp. Ford Generator

When operating F-100-250-350 trucks under conditions of excessive road splash, water may enter the generator causing failure.

To provide protection from road splash, a generator boot became effective in production on the subject trucks approximately March 15, 1963.

The new generator boot, Ford Part No. C1AZ-10170-B, can be installed on 1961-62 and on earlier production 1963 F-100-250-350 trucks equipped with the 30 amp. Ford generator when desired.

8 VINYL TRIM CLEANING MATERIALS—All Car Lines

Proper care of vinyl and soft trim parts requires the use of correct cleaning materials to assure maximum life and retention of original beauty. In this regard, two lists of cleaning materials are shown below. The first indicates those materials that are not compatible with soft trim parts and the second list indicates those materials that are.

Cleaning Materials That Should NOT Be Used

1. All materials containing aliphatic hydrocarbon or aromatic hydrocarbon solvent ingredients such as:

- Kerosene
- Naphtha
- Toluol
- Xylol 10°
- Petroleums—Heavy, Fraction, Naphtha
- Thinners—Special Lacquer
- Lacquers—Interior, Exterior
- Cellulose Acetate
- Butyl Cellosolve
- Spot Remover

2. Body polish, battery acid, anti-freezes, gasoline, motor oils or other type lubricants.

3. In general, household cleaners containing organic solvents or abrasives should not be used on soft trim parts that are color coated (leather, painted vinyls, etc.).

Cleaning Materials That Can Be Used

1. Rotunda Convertible Rear Window Cleaner (R 110-A).

Considered acceptable for cleaning and removing minute scratches from convertible back windows (available in an economical 8 oz. plastic squeeze bottle).

2. Rotunda Cleaning Concentrate (R 119-B).

Recommended for cleaning vinyl and leather trim, white side wall tires and convertible and landau tops (packaged in a 32 oz. container).

3. Rotunda All-Purpose Cleaner (R 119-A).

Recommended for cleaning fabrics, convertible and landau tops, vinyls, tires and also painted surfaces (packaged in a gallon container).

4. Rotunda Triple Clean (R 118-A).

A multi-purpose cleaner suitable for cleaning leather, vinyl, cloth, convertible and landau tops, and carpet fabrics (packaged in a 12 oz. plastic squeeze bottle with an attached brush applicator).

5. Rotunda Deep Clean (Foam Cleaner) (R 118-B).

Considered as a multiple type cleaner for fabrics and vinyls (packaged in a 32 oz. container).

NOTE: Specific instructions are provided with each of the above containers.

9 STEERING LINKAGE SERVICE REQUIREMENTS ON 1963 THUNDERBIRD AND FALCON

The steering connecting and tie rod ends on the subject vehicles are permanently lubricated and sealed during assembly. Any additional lubricant will result in an over-lubricated condition and possible seal failure.

The tie rod ends on Thunderbirds and all steering linkage on early produced Falcons have plugged holes for initial fill only. (On later produced vehicles the lube plugs have been omitted.) These ends should not be lubricated in service. In case of seal and/or other type failure, the complete part should be replaced.

Early publications of Falcon owner manuals recommended that steering linkage be lubricated at 36,000 miles.

Owners requesting this work should be advised that the steering linkage is permanently lubricated and the necessity for this operation eliminated.

10 DISC WHEEL NUT LOOSENING—Ford 500 Through 800 Series Trucks

Retaining nuts on Ford 500-800 series truck disc wheels will loosen if not properly tightened. Correct torque for these wheel nuts is 450-500 ft. lbs., and only wheel nuts which are tightened to this specification will remain tight under vehicle operation.

For proper tightening, a 500# capacity torque wrench (any one of many models offered by Snap-On, Proto, Sturtevant, Richmond, etc.) should be used. In the absence of such wrenches, the wheel nuts can be tightened to approximately correct specifications by use of an extended lever wrench. The full weight of a 150 pound man at the end of a 3 foot or 3½ foot wrench bar (held horizontally) will produce 450-500 ft. lbs. (See Figure 1).

Truck owners and operators should be cautioned that tire replacements made on the road will require the use of an extension pipe to the wheel wrench, and that as soon as possible after such repairs, a recheck of wheel nut torque with a torque wrench should be made to confirm the nut tightness. The importance of wheel nut tightness cannot be over emphasized. Truck owners should be referred to the Operator's Manual which specifies that after delivery, after any wheel replacement, after tire replacement and after cross-switching of tires, the wheel nuts should be inspected and tightened twice within the first 500 miles of operation and at the 1000 mile point after delivery or after any service requiring removal and reinstallation of wheels.

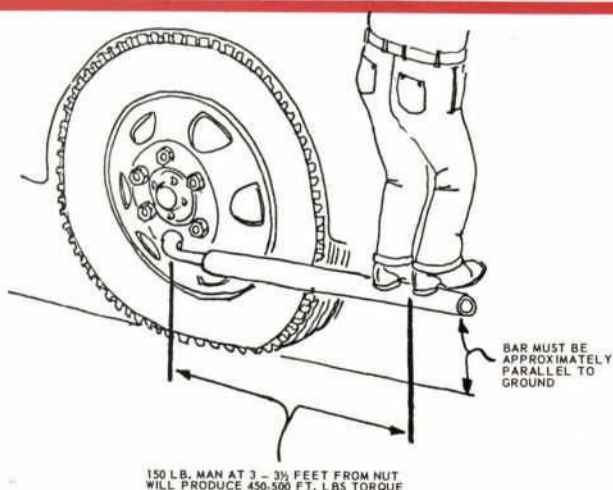


Fig. 1—500-800 Series Truck Wheel Nut Tightening Emergency Procedure

11 REVISIONS IN REAR AXLE BOLT TORQUE SPECIFICATIONS—1963 Vehicles

To keep you informed on the latest changes in rear axle component torque

specifications, the following chart indicates the bolt torque changes and the vehicles affected.

NOTE: Caution should be exercised not to exceed the maximum torque limits specified—to do so may result in thread stripping.

13 DISTRIBUTOR MODIFICATION FOR IMPROVED LOW END ACCELERATION AND FUEL ECONOMY AND CARBURETOR MODIFICATION FOR IMPROVED FUEL ECONOMY—1963 Ford with 352 Engine and 2V Carburetor

To improve low end acceleration and to improve fuel economy on the 1963 Ford with 352 engine and standard or automatic transmissions, the following Distributor or Carburetor Modifications can be made:

1963 REAR AXLE COMPONENTS—TORQUE SPECIFICATION REVISION CHART (Non Lubricated Thread) (FIGURES SHOWN IN FT.-LBS.)

Bolts Affected	Ford, Fairlane 289 4V, Thunderbird, Econoline with 2700 Axle and F-100		Fairlane (Except 289 4V)		Falcon 144, 170 CID Engine and Econoline with 2300# Axle and 144, 170 CID Engines	
	From	To	From	To	From	To
Ring Gear Bolts	65-75	65-80	65-75	65-80	40-50	40-55
Pinion Retainer Bolts	30-40	30-45	30-40	30-45
Diff. Brg. Cap Bolts	70-80	70-85	55-65	55-70	40-50	40-55
Adjuster Lock Bolts	12-20	12-25	12-20	12-25	12-20	12-25

1. Distributor Modification for Improved Low End Acceleration & Fuel Economy—Units built prior to January 19, 1963

The C3AZ-12127-AH distributor used on 390 cubic inch engines became effective in production approximately January 19, 1963, on 1963-352 cubic inch engines. This new distributor improves the low end acceleration and also improves the fuel economy when the vehicle is operated under normal load.

To improve the low end acceleration and fuel economy on cars—with 352 engines—built prior to January 19, 1963, the existing distributor can be reworked to incorporate the improvements of the new distributor by installing new primary and secondary distributor weight springs, a new vacuum diaphragm spring and a new vacuum advance stop listed below; and also adjusting the distributor advance curve to that shown in Table 1 (see next page).

The new primary and secondary distributor centrifugal weight springs—Figure 1 (next page)—increase the rate of advance during acceleration or when there is a heavy load on the engine. When the engine is operated under a light load, the new vacuum diaphragm spring—Figure 2, provides additional advance which is required for maximum part throttle power and economy. The vacuum advance stop—Figure 2—is required to limit the maximum spark advance.

12 EXHAUST SYSTEM CLEARANCE—1963 Falcon with V-8 Engine

Exhaust system alignment is an important factor in preventing noises from entering the passenger compartment.

When making replacements, the following dimensions should be maintained as closely as possible with the exhaust system cold.

1. The muffler to rear spring shackle clearance is $1\frac{1}{16}$ " on all cars with V-8 engines except Sprint. On Sprint cars the clearance should be $\frac{7}{8}$ ".

2. Muffler to fuel tank clearance is $\frac{3}{4}$ " on all cars with V-8 engines except Sprint. On Sprint cars the clearance should be $1\frac{5}{16}$ ".

3. In the area opposite the hand brake lever there must be a clearance of $1\frac{1}{4}$ " between the floor pan and muffler inlet pipe.

4. A clearance of $1\frac{1}{8}$ " to the floor pan and the engine rear mount rubber should be maintained at the engine rear mount.

5. The muffler inlet tube should have a clearance of $\frac{1}{2}$ " at the bottom rear right hand corner of the automatic transmission.

6. There should be $\frac{1}{2}$ " clearance between the muffler "Y" pipe and the starter (at the point pipe curves around the starter).

7. A clearance of $\frac{1}{2}$ " should be maintained between the flat on the muffler "Y" pipe and the power steering hoses.

The above areas are indicated in Figure 1 for clarification of location.

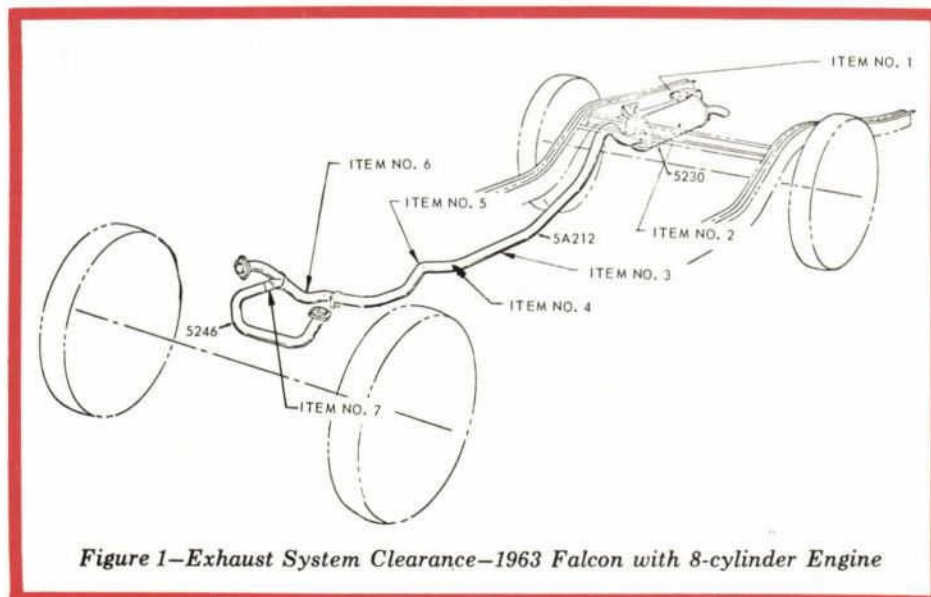


Figure 1—Exhaust System Clearance—1963 Falcon with 8-cylinder Engine

Ford Part Number and Name	Required Quantity
B8A-12192-B Primary Weight Spring (color code—orange)	1
B7A-12191-B Secondary Weight Spring (color code—green)	1
C0TZ-12192-A Vacuum Diaphragm Spring (color code—blue)	1
C0TZ-12202-A Vacuum Advance Stop	1

2. 2V Carburetor Modifications for Improved Fuel Economy

A. Booster Venturi—1963

Fuel economy during off idle throttle operation can be improved by replacing the booster venturi assembly (C1AZ-9A523-C) with a new assembly, part number C0AE-9A523-A. This improved booster venturi is calibrated with a smaller idle-fuel mixture restrictor, and will reduce the fuel-air mixture in the idle system during off-idle throttle operation. The booster venturi can be used in carburetors with either manual or automatic transmission; carburetors built with the satisfactory booster can be identified by a dot of orange paint on the code tag.

B. Main Metering Jet (one size leaner) —1960 through 1963 units built prior to November 2, 1962

Fuel economy under normal driving conditions can be improved by leaning the part throttle and wide open throttle flow characteristics of the 2V Ford carburetor by changing the main metering jet to a leaner size.

New carburetors with one size leaner (smaller) main metering jets became effective in production approximately November 2, 1962. Carburetors incorporating this change can be identified by the letter "B" stamped in the carburetor code tag after the prefix and suffix.

The part numbers of the leaner main metering jets, and their application are as shown in Table 2.

TABLE 1

Centrifugal Advance: Set test stand to 0° @ 250 RPM and 0 inches of vacuum.

Distributor RPM	Advance (Degrees)	Vacuum (Inches of Mercury)
400	½—1½	0
500	3½—4½	0
600	5—6	0
1100	7—8¼	0
2000	10¼—12¼	0

Vacuum Advance: Set test stand 0° @ 1000 RPM and 0 inches of vacuum.

Distributor RPM	Advance (Degrees)	Vacuum (Inches of Mercury)
1000	½—3½	7
1000	3½—6½	10
1000	5½—8½	12
1000	5½—8½	20

TABLE 2

Part Number	Jet Size and Identification Number	Application
C1AZ-9533-D	56	0 to 5,000 ft. Std. Trans.
C1AE-9533-A	54	5,000 to 10,000 ft. Std. Trans.
C1AZ-9533-L	52	10,000 to 15,000 ft. Std. Trans.
C1AE-9533-B	55	0 to 5,000 ft. Auto. Trans.
C1AZ-9533-H	53	5,000 to 10,000 ft. Auto. Trans.
C1AZ-9533-M	51	10,000 to 15,000 ft. Auto. Trans.

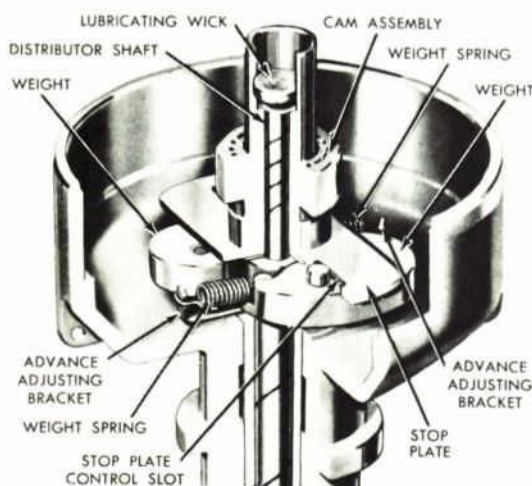


Figure 1—Centrifugal Advance Mechanism

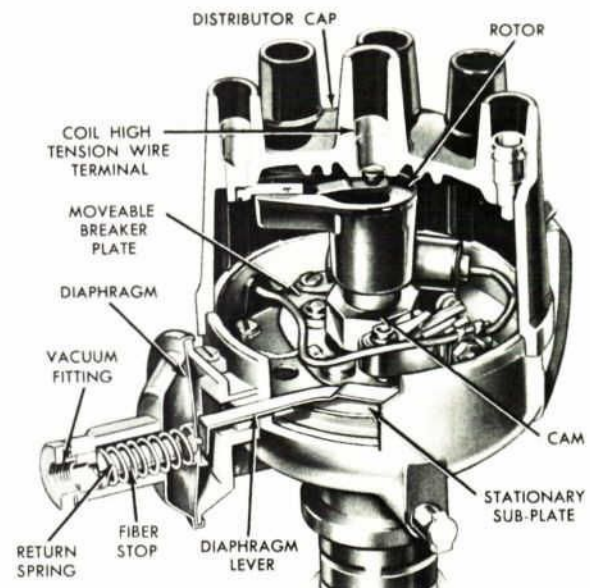


Figure 2—Vacuum Advance Mechanism

14 INCREASED ENGINE IDLE SPEED, 1963-144-170 CID Passenger Car Engines with Automatic Transmissions

In order to maintain a smoother and more stable idle, it is recommended that the idle speed be increased on the 1963 144-170 passenger car engines with automatic transmissions.

The specifications for engine idle speed were revised early in 1963 as shown below:

144-170 CID Engine	Automatic Transmission	500-525 RPM (was 475-500)
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15 HYDRAULIC TAPPET NOISE—DIAGNOSIS AND TESTING—All Car Lines

Whenever hydraulic tappet noise is encountered and a problem of engine oil aeration is suspected, the following diagnosis procedure is recommended. It may save some time by eliminating engine tear-down for inspection:

1. Check the engine oil for proper level and correct as required. Too high a level may cause aeration by crankshaft splash. Also check the dipstick to assure the correct part is being used.

2. Remove engine oil pressure sending unit, and insert a petcock type valve that will permit a 1/4 to 3/8 inch hose to be attached. Use a sufficient length of hose, so that the oil may be returned back into the oil fill tube. Transparent tubing is desired. Close this valve.

3. Operate the engine at approximately 1200 RPM until "normal" engine temperature is indicated.

4. Bring down engine speed to approximately 500 RPM and open petcock *slightly* to permit a steady oil discharge and observe for air bubbles.

5. Increase engine speed to approximately 1000 RPM and recheck for air bubbles. To facilitate observation, direct the oil flow over a white card or through transparent tubing.

NOTE: The engine should not be operated at excessive speeds or for extended periods with the above oil bleed.

If evidence of aeration is present, the engine oil pan should be removed and the pump and intake system closely inspected. The difficulty may be at either end of the pick-up tube assembly (pin hole or defective weld), the gasket between the pick-up tube and pump body, or a cracked oil pump body. Correct as necessary.

16 NEW CYLINDER HEAD GASKET, HEAD BOLT WASHERS AND HEAD BOLT SPECIFICATIONS—1958 Through 1963 Truck—401, 477, 534 Engines

On complaints of abnormal coolant loss in super duty engines, it is imperative that repairs be made immediately. Investigations have shown that in some instances repairs have been delayed until major damage or complete engine replacement is required.

The new rubber-asbestos composition head gasket (Ford Part No. C3TZ-6051-F) should be used for all service replacements. Along with the composition gasket, it is mandatory that the new flat washers (Ford Part No. 378682-S) be used under the cylinder head bolts.

The new washers replace the earlier concave type.

Prior to installing the new gaskets it is recommended that the cylinder head bolt holes in the block be cleaned, using a bottoming tap, and then blown out with compressed air. This will prevent false torque reading on the cylinder head bolts due to accumulation of varnish and foreign material in block holes. Cylinder head bolt threads should also be cleaned

and oiled. Gasket sealer is not used with the composition-type gasket.

17 SURGING OR HESITATION—1963 Econoline with 144 or 170 Engine

Vehicle surging or hesitation at part throttle steady speed or wide open throttle operation, caused by an excessively lean fuel mixture may be encountered on 1963 Econolines with both the 144 and 170 engines. Design specifications for the carburetor favor the lean side for fuel economy but under certain operating conditions may affect smooth engine operation.

The carburetor can be modified to correct the lean mixture and surging problem by installing a main metering jet one number size larger and by changing the power valve timing to open sooner (at less throttle opening).

The power valve timing change can be accomplished by installing four additional calibrating shims (Ford Part No. 375910-S) on the power valve rod, see Figure 1. Under no condition should the total number of shims exceed 8, as fuel economy will be adversely affected. If more than 4 shims exist on the power valve rod as installed in production, then fewer additional shims should be used so that the total amounts to only 8 shims.

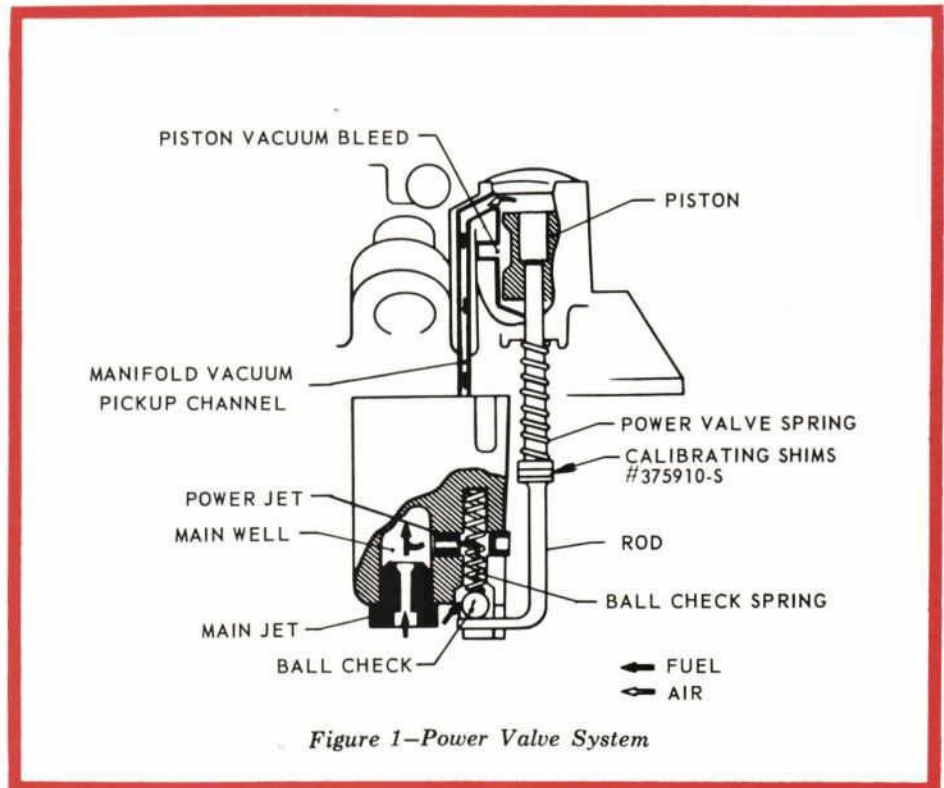


Figure 1—Power Valve System

18 CLUTCH SNAP RING FAILURE
—All Fordomatic Two-Speed
Transmissions

Clutch plate failures on Fordomatic two-speed transmissions can be caused by failure of the snap ring which retains clutch pack and sun gear in the clutch drum. See Figure 1. This snap ring may have lost its tension due to

the influence of high temperature, and may come free from the retaining groove in the clutch drum. This allows the forward sun gear to move out of the drum with a resultant loss of compression and slippage of the clutch pack upon piston application.

Transmissions built after July, 1963, have snap rings which are not subject to this tension loss.

On transmissions built before Au-

gust, 1963, which encounter clutch failure, the snap ring existing in the assembly should not be reused. A new snap ring (Ford Part No. B9A-77523-A) should always be installed. Furthermore, subsequent failure of the clutch pack because of this snap ring can be prevented by making it a practice to replace this snap ring whenever the transmission is disassembled for any internal repairs.

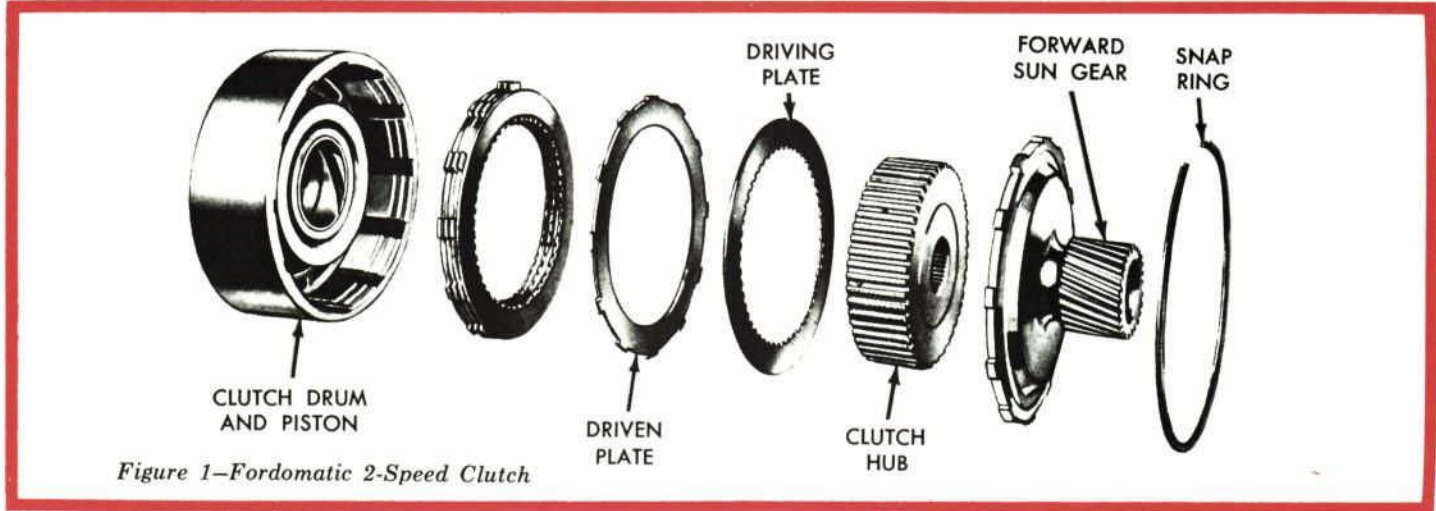


Figure 1—Fordomatic 2-Speed Clutch

19 CLUTCH SNAP RING FAILURE
—All 1961 Through 1963
Cruise-O-Matic Transmissions
for 223, 260, 289, 292, and
352 CID Engines

Clutch plate failures on Cruise-O-Matic transmissions can be caused by failures of one or all of the following snap rings: the input shaft to front clutch cylinder snap ring, the front clutch release spring to front clutch

cylinder snap ring and the rear clutch pressure plate snap ring. See Figure 2. These snap rings may have lost their tension due to the influence of high temperature, and may come free from the retaining groove in the clutch cylinder and/or drum. This allows the clutch pressure plates (front or rear) and/or clutch release spring to move out of the cylinder or drum with a resultant loss of compression and slippage of the clutch pack upon piston application.

On transmissions built before mid-August, 1963, which encounter clutch failure, the snap rings existing in the assemblies should not be reused. New snap rings should always be installed. Furthermore, subsequent failure of the clutch packs because of these snap rings can be prevented by making it a practice to replace these snap rings whenever the transmission is disassembled for any internal repairs.

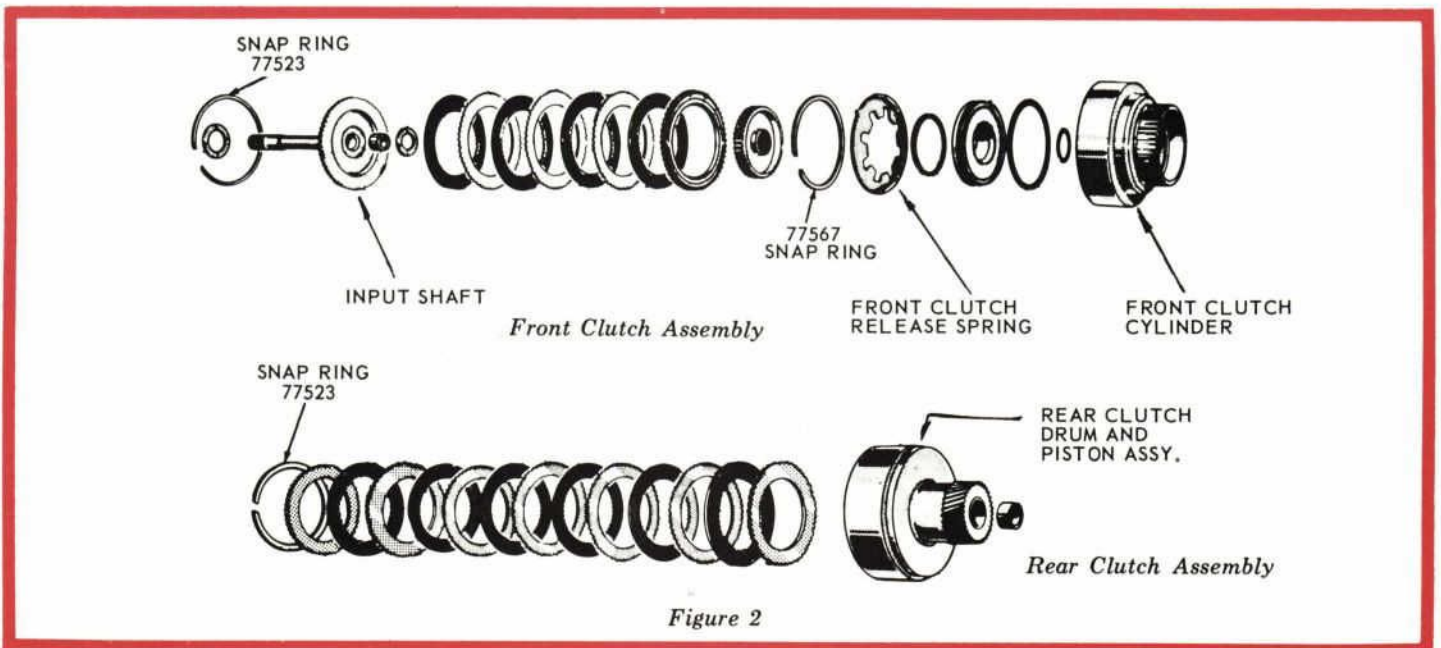


Figure 2

20 CARBURETOR PERCOLATION OR EXCESSIVE PRESSURE BUILD-UP IN FUEL LINE—

All 1954-62 Six & Eight Cylinder Passenger Cars Without Pressure Bleed Pumps

Hard hot engine starting is generally caused by fuel percolation in the carburetor main well, or excessively high pressure build-up in the fuel line between the pump and carburetor. The high pressure build-up results from the hot soak period. The percolation is aggravated by the highly volatile fuel and the retention of pressure in the fuel line.

In the event that percolation takes place, fuel is discharged into the induction system causing the fuel level to drop, thereby permitting additional fuel to be forced into the fuel bowl by the residual pressure in the line. It can be seen that a full pump-stroke of fuel

may be discharged into the intake manifold by this sequence of events.

In the event excessively high pressure is built up in the fuel line, the problem of hard hot starting is due to the inability of the fuel inlet system to withhold the abnormally high pressure and fuel is forced past the fuel inlet needle, thereby raising the fuel level and causing the carburetor to flood over into the induction system.

Thus, where normal carburetor adjustments do not alleviate the problem, the difficulty can be greatly minimized, and in most cases eliminated by incorporating a pressure leakdown bleed between the pressure and inlet side of the fuel pump. This will reduce the amount of available fuel that can be forced into the carburetor after engine shut down. It has been determined that the bleed hole must be a minimum size—.0135" in diameter, a number 80 drill.

On A/C type fuel pumps the bleed hole can be drilled in the wall directly

over the inlet valve cavity. See Fig. 1.

On Carter design fuel pumps, the bleed hole can be drilled into the fuel outlet passage wall, located on the low pressure side of the valve body. See Figure 2.

On some Carter models it may be necessary to drill the bleed hole in the web, on the pulsator side of the valve body, which separates the inlet and pressure cavities.

Specific location of the bleed hole is not critical as long as it is located between the inlet and pressure side of the pump. The diameter of the bleed hole is very critical however, and under no circumstances should a larger hole than specified be drilled.

When this problem is encountered, it is suggested that this pressure relief bleed-hole be incorporated in the fuel pump to minimize hard hot engine starting, as previously described.

This bleed hole is incorporated in the current production fuel pumps in all vehicles encountering this problem.

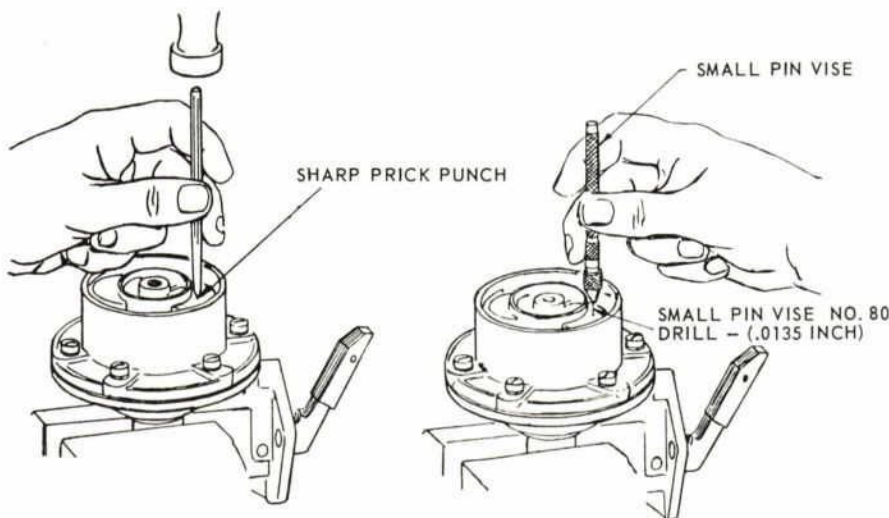


Figure 1—Bleed Hole—A/C Type Fuel Pump



Figure 2—Carter Pump

21 SPARK PLUG FLASHOVER DURING COMPRESSION TEST ON SPARK PLUG TESTERS

Spark plug flashover is the electrical sparking from the spark plug terminal down the insulator to the ground on the metal shell.

This condition in itself does not indicate a defective spark plug. In fact it indicates that the plug insulator is in good condition in that it has no cracks or pin hole punctures that could cause spark plug misfire.

This flashover will not occur in engine operation where proper fitting ignition cable boots which are in good condition are used. It can be observed in some compression testers which are

affected by atmospheric and humidity conditions. Therefore, to avoid the possibility of encountering this condition of flashover when testing spark plugs in a compression tester, the tester can be fitted with an ignition cable boot. A 6 to 8 inch section of wire core ignition cable with a 90° molded boot connected to the clip on the tester should provide a suitable adapter.

22 SPARK PLUG REPLACEMENT—1962 & 1963 Fairlane with 221 and 260 Cubic Inch Eight Cylinder Engines

The following guide is recommended

when spark plug replacement becomes necessary on 221 or 260 cubic inch eight cylinder engines in the subject unit.

Type of Operation Condition	Ford Part No. Recommended Spark Plug
Normal and/or Severe Service	B8A-12405-A (BF 42)
Light Service—Excessive Idling—Stop and Go City Driving	B7A-12405-B (BF 82)

23 DISTRIBUTOR TESTING OF TRANSISTOR IGNITION—427 High Performance and Super Duty Truck Engines—1963

One of the desirable features of Transistor Ignition is the absence of pitting or ignition contact-point contamination. This is possible because of the low current and voltage requirements of the system. However, when checking the transistor ignition distributor on a test machine, the conventional system hook-up may cause point contamination.

The extent of this contamination is dependent upon the amount of time the distributor is run in the test machine. Extended testing will cause a definite amount of pitting. Therefore, it is recommended following such a test, that a point contact cleaner or solvent be used to remove any oxidation that is present. These cleaners are available in any radio supply store.

Since there is no condenser in the transistor ignition distributor, it will be necessary to incorporate one in the circuit when using a distributor test machine.

Figure 1 illustrates one manner in which this may be accomplished. Any of the current Ford distributor condensers can be used, since both car and truck have the same capacity. This is 0.21 to 0.25 microfarads.

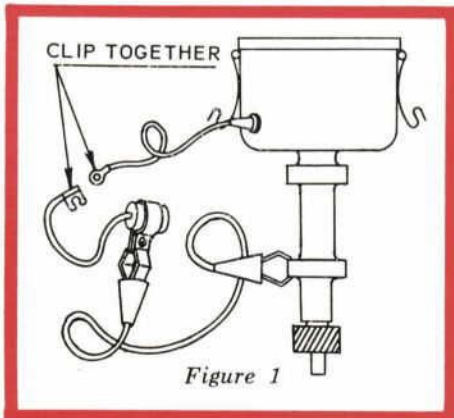


Figure 1

24 SERVICE REPLACEMENT RADIO SPEAKERS—

Ford Cars and Trucks

Separate radio speakers are now available to service Ford cars and trucks as follows:

Part Number	Application
C3SZ-18808-A	1963 Thunderbird
C3MY-18808-A	1963 Ford Galaxie
C2YY-18808-A	1963 Falcon, 1962 & '63 Fairlane
C1TZ-18808-A	1961-62-63 Truck
C1UZ-18808-A	1961-62-63 Econoline

25 INSTRUMENT PANEL GAUGE READINGS—All 1963 Vehicles with AM-FM Radio

All vehicles having combination AM-FM radios are equipped with a radio suppression choke that connects to the ignition side (input) of the constant voltage (C.V.) regulator.

However, the terminal of the suppression choke is such that it can be installed on the gauge side (output), resulting in low gauge readings.

Before making gauge tests and/or replacements to the fuel, oil pressure, and temperatures systems on vehicles equipped with AM-FM radios, check the radio suppression choke to be sure it is connected to the ignition side (input) of the C.V. regulator. See Fig. 2.

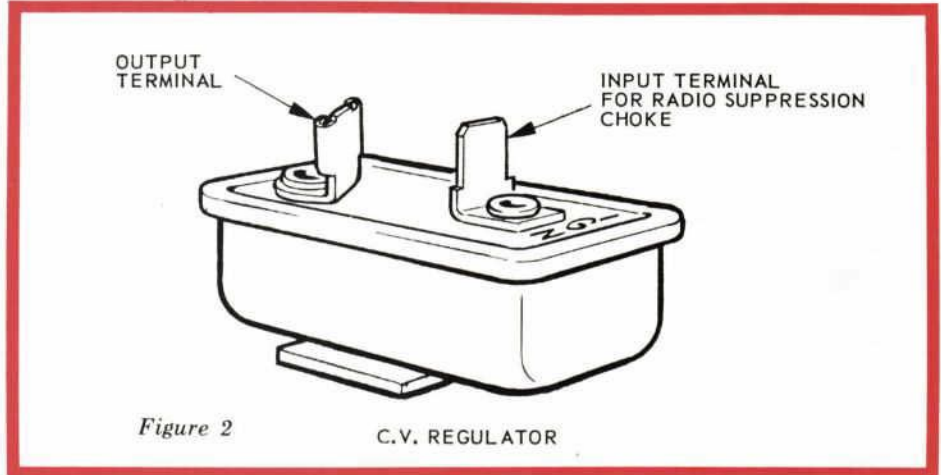


Figure 2

C.V. REGULATOR

26 RADIO CONTROL BREAKAGE—TONE, VOLUME, ON-OFF SWITCHES—All 1963 Vehicles

Examination of samples of the above knobs indicates that many failures are due primarily to damage. The damage and resultant failures are attributed to the neglect of the mechanic in removing the broken control knob pin from the control assembly prior to installing a new control knob.

The broken control knob pin can easily be removed from the control cavity by bending a paper clip to form a small hook on one end. Insert the hooked end into the center of the broken pin and pull outward to remove. See Figure 3.

ing the broken control knob pin from the control assembly prior to installing a new control knob.

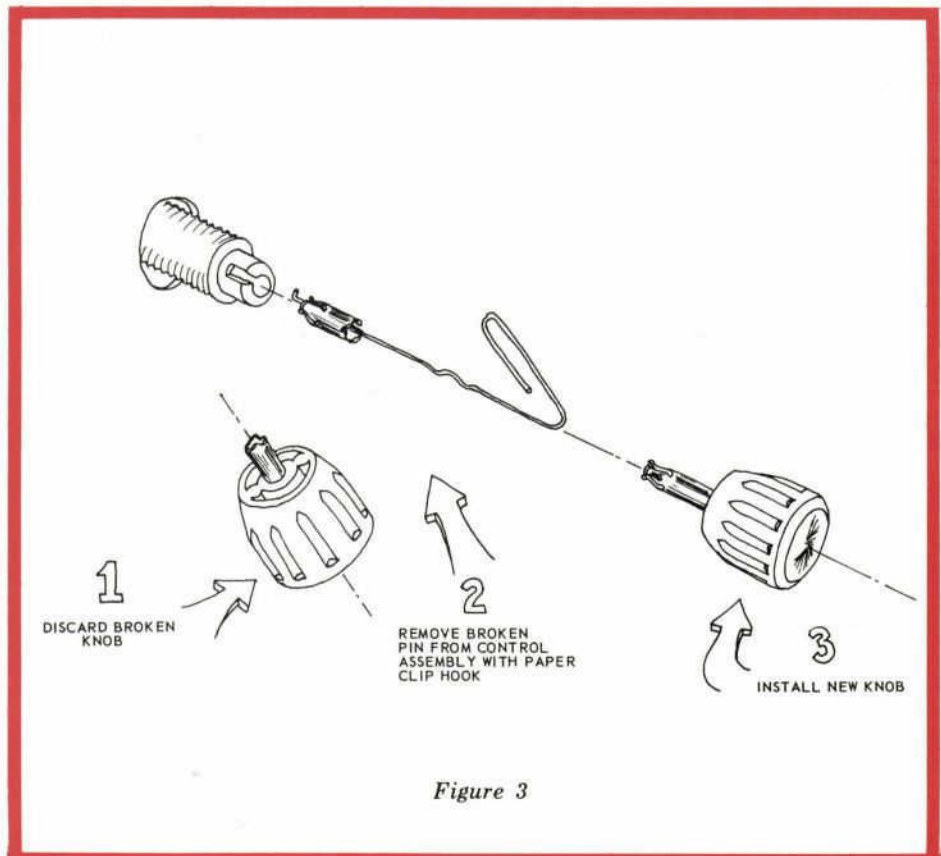


Figure 3

27 LOOSE TACHOMETER HEAD —1963 Falcon Sprint

Loose tachometer heads and mounting plates have been encountered on 1963 Falcon Sprints built prior to May 1, 1963. The loose heads are caused by loss of torque of the adjusting screw and are usually found on vehicles without a crash pad. This can be corrected by the addition of one #8 tooth lockwasher as shown in Figure 1.

A loose mounting plate on a vehicle with a crash pad is caused by the compressibility of the crash pad material. This has been corrected by use of a spacer that will give solid support to the mounting plate.

Vehicle without crash pad can be corrected by:

Adding one #8 tooth lockwasher to the tachometer mounting bracket screw as in Figure 1. Ford Part Number 34902-S7 (internal) or 34951-S (external) countersunk lockwasher will suffice.

Vehicle with crash pad can be corrected as follows:

1. Remove tachometer and mounting bracket.
2. Cut a $\frac{1}{4}$ " length of $\frac{3}{8}$ " O.D. copper tubing to be used as a spacer at rear mounting hole.

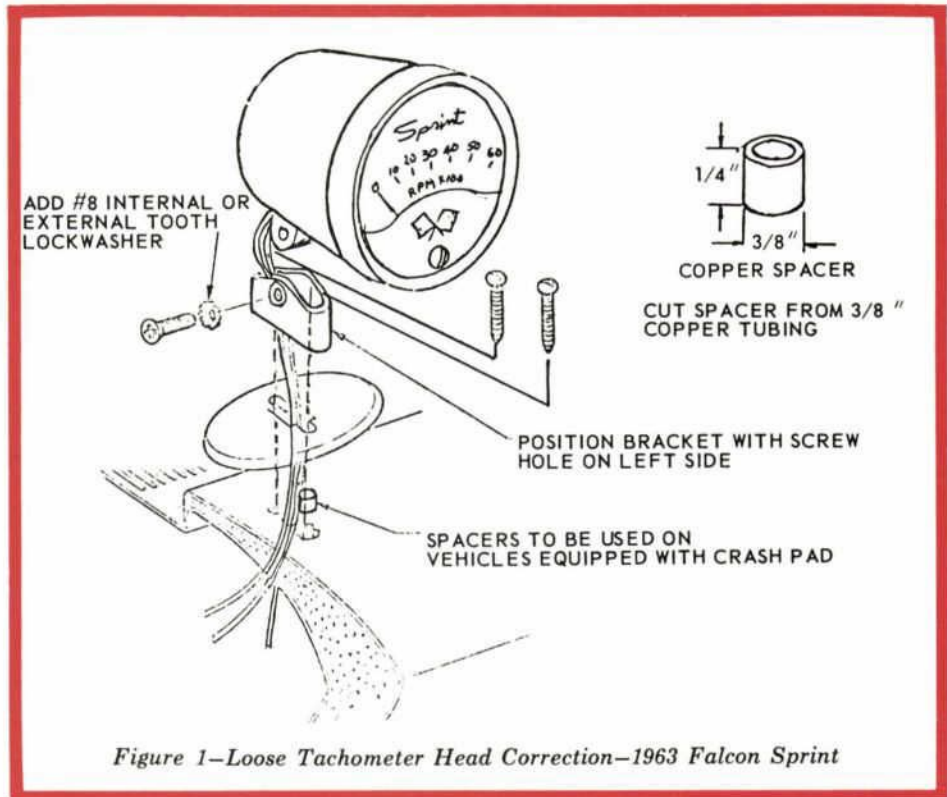


Figure 1—Loose Tachometer Head Correction—1963 Falcon Sprint

3. Cut out crash pad vinyl and foam around rear instrument panel hole to permit spacer to seat onto instrument panel metal.

4. Position mounting bracket so retaining screw can be installed from the left-hand side. Align spacer to rear mounting hole (hole furthest from

windshield) and install bracket.

5. Attach tachometer head to mounting bracket using a #8 tooth lockwasher as outlined for vehicles without crash pad. The #8-32 x $\frac{1}{2}$ flathead screw that holds tachometer head to bracket must be installed from left-hand side.

28 TACHOMETER INSTALLATION ON STANDARD IGNITION ENGINES

The Instruction Sheet (I.S. 1005) included with early C3RZ-17A326-A and B Rotunda Tachometer Kits may be misleading.

To operate correctly, the Rotunda tachometer must be connected in series with the ignition circuit. This is accomplished by disconnecting the ignition resistor wire (pink) from the ignition switch. The tachometer is then connected into the circuit in series (red wire to ignition switch and black wire to the free end of the pink resistor wire). *The tachometer black wire should NOT be connected to the distributor as indicated in I.S. 1005.*

The blue wire from the tachometer is the illuminating bulb feed wire and should be connected into the instrument panel lighting circuit as shown in the instruction sheet.

On transistorized ignition systems, a shunt wire is required as shown in Figure 2.

29 TACHOMETER APPLICATION TO TRANSISTORIZED IGNITION SYSTEM— All Vehicles

Failure of a tachometer can occur on vehicles equipped with a transis-

torized ignition system because of the higher current draw of these systems. This is true of all transistor systems.

To prevent these failures, a shunt circuit should be installed across the tachometer leads as shown in Figure 2. This shunt can be fabricated from 10" of Ford Part No. COLF-12250-A ignition resistor (pink) wire.

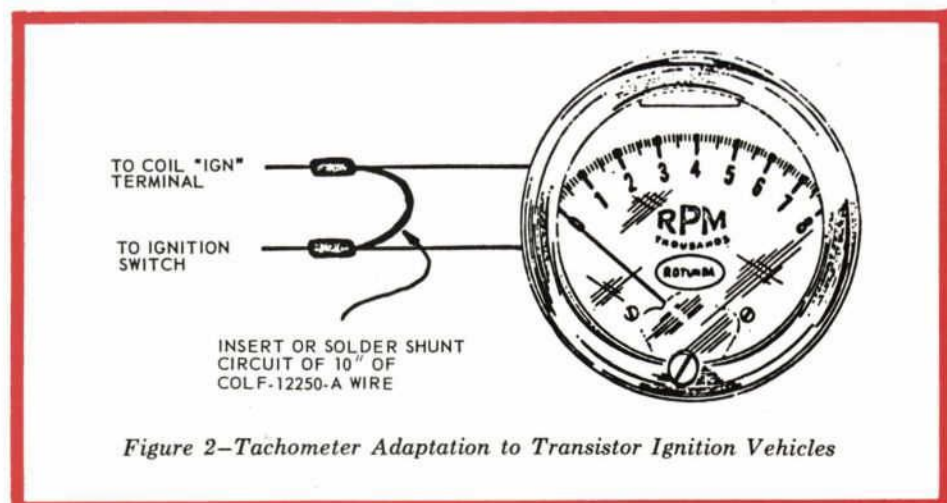


Figure 2—Tachometer Adaptation to Transistor Ignition Vehicles

**30 TURN SIGNAL SWITCH NOT CANCELLING—
1963 Ford with Automatic Transmission**

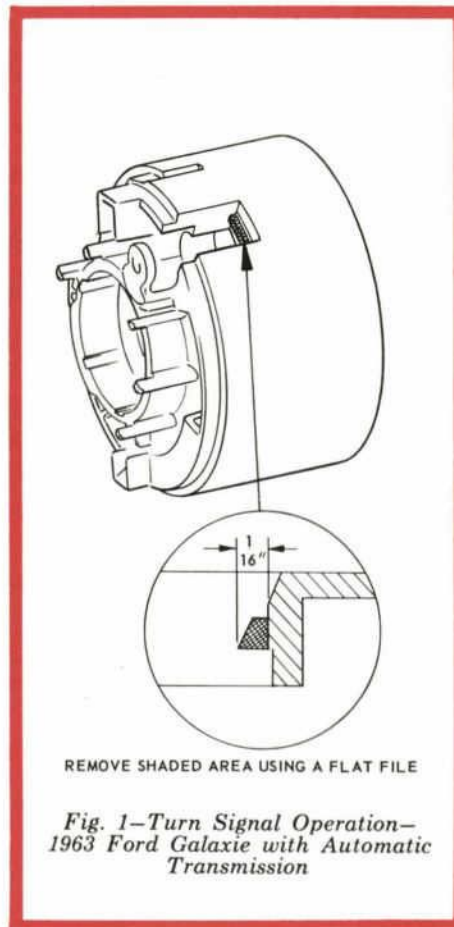
Problems with turn signal switches not cancelling and/or having high operating effort may be due to the turn signal lever binding on the steering column tube and pin flange assembly.

Where this condition is encountered, remove the turn signal lever. Insert a piece of cloth in the turn signal slot. Using a fine mill file, remove the shaded area shown in Figure 1. Reinstall the turn signal lever handle and check the turn signal operation. If the switch still does not cancel properly, replace it. Use switch, Ford Part No. C3AZ-13341-C for fixed steering columns and C3AZ-13341-D for moveable steering columns.

**31 SEAT BELTS (METAL TO METAL TYPE)—
Proper Threading Through Buckle or Hook Assembly—
1963 Vehicles**

Proper threading of the seat belt through the buckle and/or hook is essential for providing positive tension resistance and proper holding capacity.

Figures 2 and 3 are provided to illustrate proper threading of the belts. Be sure to follow them.



*Fig. 1—Turn Signal Operation—
1963 Ford Galaxie with Automatic Transmission*

**32 FUEL LINE VIBRATION (FUEL PUMP TO CARBURETOR)—
1963 221, 260 and 289 C.I.D. V-8 Engines**

Fuel line vibration and resultant failure of the line between the fuel pump and the carburetor can occur on vehicles equipped with the subject engines; particularly when operating on rough surfaced roads. For this reason, a fuel line bracket was used in late 1963 production and has been made available for correcting such failures and reducing fuel line vibration.

The following pieces are required for this installation:

Qty. Reqd.	Ford Part No.	Description
1	C30Z-9180-A	Bracket Assy.
1	354342-S8	Clip—Fuel Line to Bracket
1	370003-S8	Screw—10-32 x .69 Pan Head Locking

The bracket is to be installed on the water pump upper retaining bolt as shown in Fig. 4.

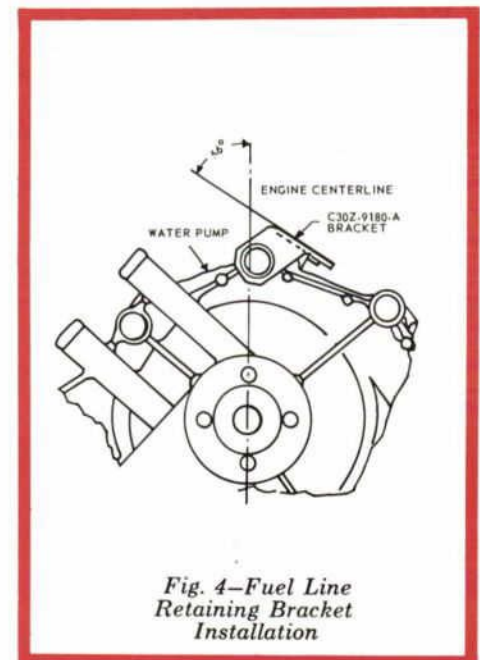


Fig. 4—Fuel Line Retaining Bracket Installation

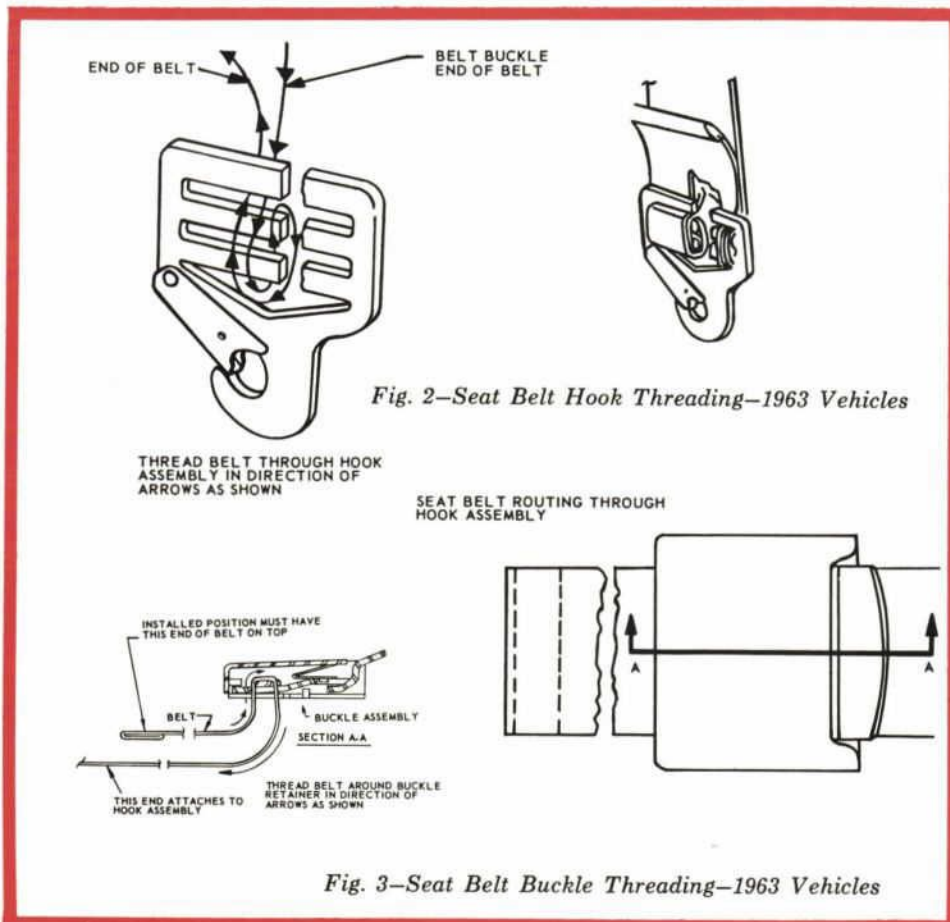


Fig. 2—Seat Belt Hook Threading—1963 Vehicles

Fig. 3—Seat Belt Buckle Threading—1963 Vehicles



33 IMPROVED AUTOMATIC CHOKE OPERATION AND FUEL ECONOMY ON SHORT TRIP STOP AND GO TYPE DRIVING—221, 260, 352, 390 C.I.D. Engines

Clamping the heater hose to the choke housing will improve the operation of the automatic choke system on these eight cylinder engines. The hot water in the heater hose is used to provide a source of continuing heat to the thermostatic choke spring and thus prevents excessive choking when a warm engine is restarted. Fuel economy will also be improved especially during short trip stop and go type of driving. The hot starting characteristics will also be improved with this device.

All 289 CID engines have the automatic-choke, heat retention system. This feature was incorporated in 1964 production on the 260, 352 and 390 CID engines (Refer to Fig. 1).

Early production cars that do not incorporate this desirable feature can be modified with the following procedure:

All Engines (Refer to Fig. 2)

1. Remove the carburetor air cleaner assembly.

NOTE: Vehicles equipped with the fourteen or sixteen inch air cleaner will require additional modification for heater hose clearance. Nineteen inch air cleaners do not require modification. (See Fig. 6).

2. Remove the choke cover retaining screws and install the new adaptor screws, Ford Part No. C3AZ-9B874-A. NOTE: Removing one screw and installing the adaptor screw, progressively, will make installation quick and easy without disturbing the choke setting.

221 CID and 260 CID Engines (Fairlane and Falcon) (Refer to Fig. 3).

1. Remove the choke air shield.
2. Disconnect the choke heat tube and the distributor vacuum line at the carburetor.
3. Reroute the heater inlet hose next to the choke cover.
4. Position the Clamp, Ford Part No. C3AZ-18572-A over the heater hose and choke cover. Install the clamp retaining screws, Ford Part No. 31061-S.
5. Reinstall the distributor vacuum line, choke heat tube and the choke air shield to the carburetor.

352 CID and 390 CID Engines Except Thunderbird (Refer to Fig. 4).

Due to the water-warmed carburetor spacer used on these engines, the heater return hose is used to supply the additional choke heat.

1. Remove and discard the heater outlet hose bracket from the fender shield.
2. Reroute the heater return hose next to the choke cover.
3. Position the clamp (Ford Part No. C3AZ-18572-A) over the heater hose and choke cover. Install the clamp retaining screws (31061-S).

390 CID Engine (Thunderbird) (Refer to Fig. 5).

A thermostatic valve controls the coolant flow in the Thunderbird heater system. Therefore, new hose lengths and routing will be required to by-pass the valve and provide an uninterrupted flow of heated coolant for proper choke operation.

1. Drain radiator coolant.
2. Remove and discard the carburetor heat spacer outlet hose.
3. Remove and discard the heater return hose. Retain the "Y" adaptor.
4. Cut a 7 inch length of 3/4 dia. heater hose and install one end to out-

let end of the "Y" adaptor and the other end to the water pump fitting.

5. Cut a 34 inch length of 3/4 dia. heater hose and install one end to the inlet end of the "Y" adaptor. Route the hose through the fender bracket to the heater core return outlet. Install the hose to the outlet.
6. Cut a 40 inch length of 5/8 dia. heater hose and install one end to the "Y" adaptor near the water pump. Route the hose over the spark plug wires, choke exhaust heat line and heater vacuum control line and to the carburetor heat spacer return outlet. Install the hose to the outlet.

7. Position the hose to the choke cover and the hose clamp (Ford Part No. C3AZ-18572-A) over the hose and cover. Install the clamp retaining screws.

8. Band the three hoses together for support.

9. Fill radiator with coolant and check all hose connections for leaks.

10. Install air cleaner.

Air Cleaner—Fourteen and Sixteen Inch Diameter (Refer to Fig. 6).

1. Mark a line 1/4 inch from the edge of the choke relief area. Blend the line into the corners of the relief.

2. Using the ball side of a "ball peen" hammer, indent the metal in the area previously marked off to provide the necessary clearance for the heater hose.

CAUTION: Be sure not to distort or deform the air cleaner element sealing surface.

3. Position the air cleaner body over the carburetor and check for clearance at the heater hose and for proper seating of the body to the carburetor. Install the air cleaner element, cover, and choke vacuum hose to complete the installation.

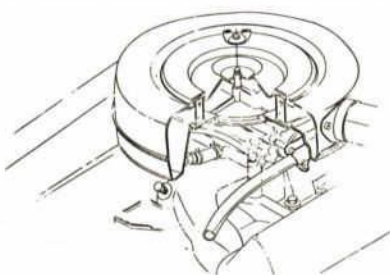


Fig. 1—Heater Hose To Automatic Choke Installation

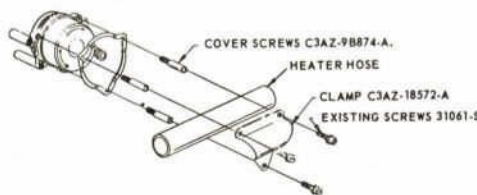


Fig. 2—Heater Hose Clamp Installation

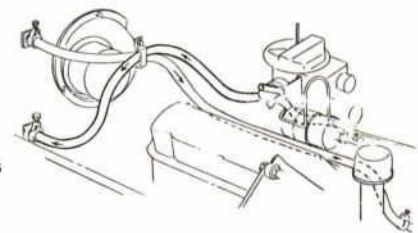


Fig. 3—221 And 260 C.I.D. Engine Heater Hose Routing

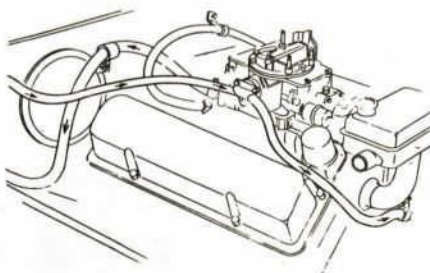


Fig. 4—352 And 390 C.I.D. Engine Heater Hose Routing

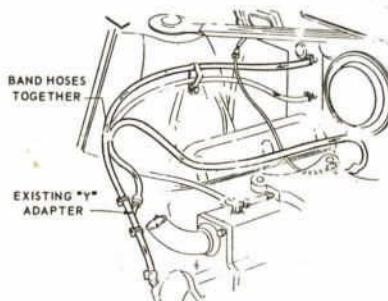


Fig. 5—390 C.I.D. Thunderbird Heater Hose Routing

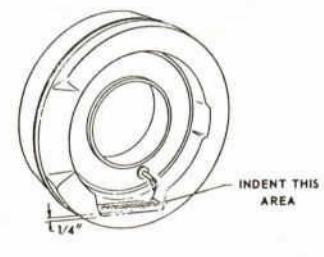


Fig. 6—Air Cleaner Modification